

Formulas for gears calculation – internal gears

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Meaning of symbols			
a	Center distance	m	Module
α	Pressure angle	Q	Dimension over pins or balls
β	Helix angle	r	Radius
d	Diameter	R_a	Radius to start of active profile
g	Length of contact	s	Tooth thickness on diameter d
g_1	Legth of recession	\bar{s}_{os}	Chordal thickness
g_2	Length of approach	t	Pitch
h_f	Dedendum	w	Chordal thickness over z' teeth (spur gears)
h_k	Addendum	W	Chordal thickness over z' teeth (helical gears)
h_0	Corrected addendum	z	Number of teeth
h_r	Whole depth	x	Profile correction factor
l	Tooth space		
Meaning of indices			
b	Referred to rolling diameter	n	Referred to normal section
c	Referred to roll diameter of basic rack	o	Referred to pitch diameter
f	Referred to root diameter	q	Referred to the diameter through balls center
g	Referred to base diameter	r	Referred to balls
k	Referred to outside diameter	s	Referred to transverse section
i	Referred to equivalent	w	Referred to tool

Internal spur gears with normal profile

$$d_o = m \cdot z$$

$$t_o = m \cdot \pi$$

$$d_g = d_o \cdot \cos \alpha_o$$

$$t_g = t_o \cdot \cos \alpha_o$$

$$h_k = m$$

$$h_f = \frac{7}{6} \cdot m \quad \text{or} \quad h_f = \frac{5}{4} \cdot m$$

$$h_r = h_k + h_f$$

$$d_k = d_o - 2h_k$$

$$d_f = d_o + 2h_f$$

$$s_o = \frac{m \cdot \pi}{2}$$

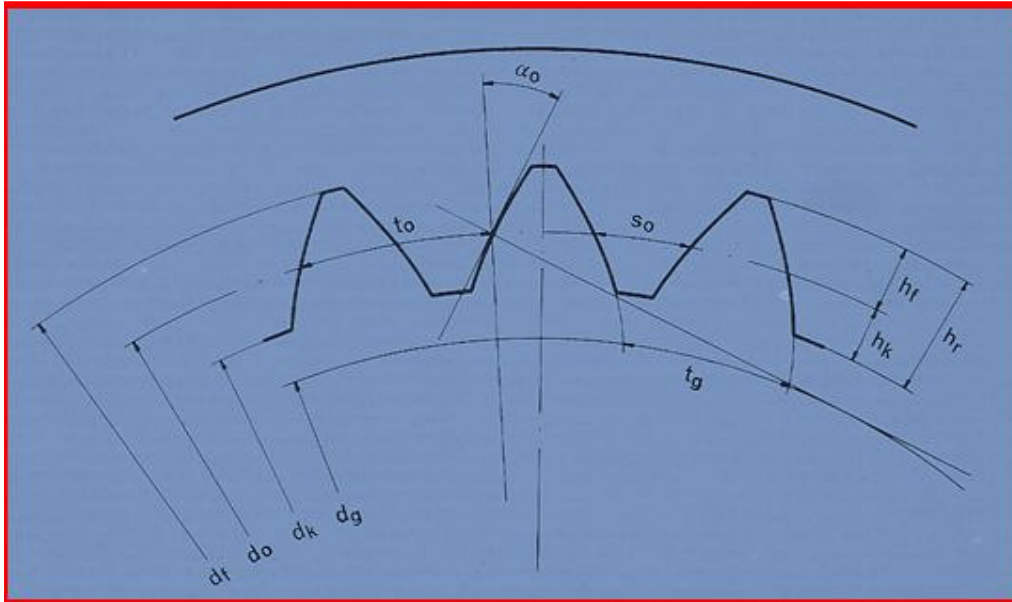
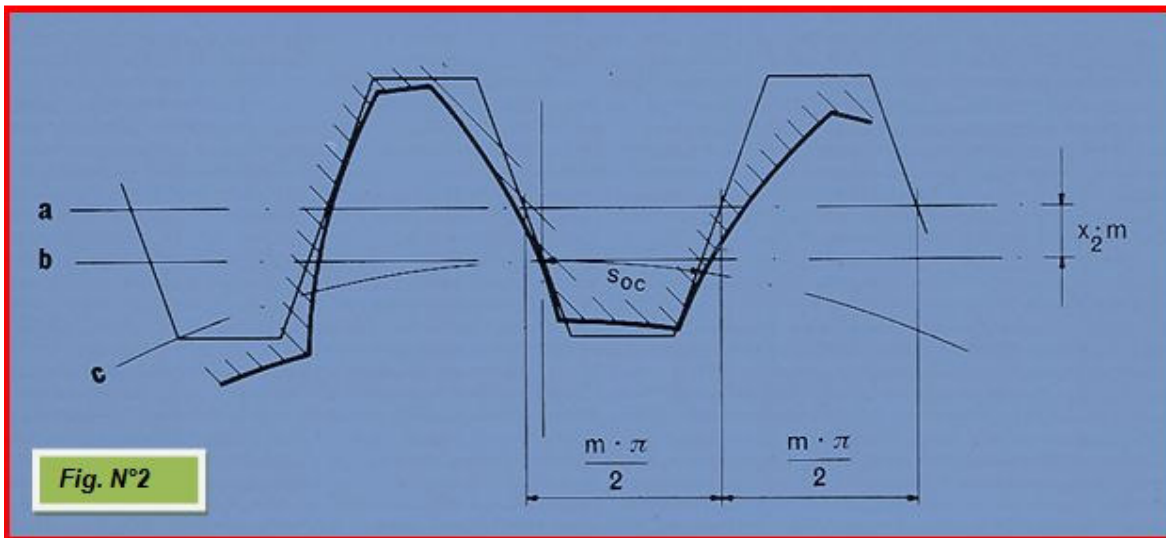


Fig.N°1

Internal spur gears with corrected profile



a)- Without center distance variation

$$h_k = m - x \cdot m$$

$$h_f = \frac{7}{6} \cdot m + x \cdot m \quad \text{or} \quad h_f = \frac{5}{4} \cdot m + x \cdot m$$

$$s_{0c} = \frac{m \cdot \pi}{2} - 2 \cdot x \cdot m \cdot \tan \alpha_0$$

b)- with center distance variation

$$\text{inv } \alpha_b = \text{inv } \alpha_0 + 2 \tan \alpha_0 \frac{x_1 - x_2}{z_1 - z_2}$$

$$a_b = a \frac{\cos \alpha_0}{\cos \alpha_b} \quad d_b = \frac{d_g}{\cos \alpha_b}$$

$$s_b = r_b \left[\frac{S_{oc}}{r_o} - 2(\text{inv } \alpha_o - \text{inv } \alpha_b) \right]$$

$$d_k = m(z - 2 + 2x)$$

Internal helical gears with normal profile

$$\begin{aligned} d_o &= m_s \cdot z & t_{os} &= m_s \cdot \pi \\ d_g &= d_o \cdot \cos \alpha_{os} & t_{gs} &= t_{os} \cdot \cos \alpha_{os} \\ m_n &= m_s \cdot \cos \beta_o & \tan \alpha_{on} &= \tan \alpha_{os} \cdot \cos \beta_o \\ t_{on} &= m_n \cdot \pi & t_{gn} &= t_{on} \cdot \cos \alpha_{on} \\ h_k &= m_n & h_f &= \frac{7}{6} \cdot m_n \quad \text{or} \quad h_f = \frac{5}{4} \cdot m_n \\ h_r &= h_k + h_f & d_k &= d_o - 2h_k \\ d_f &= d_o + 2 \cdot h_f & s_{on} &= \frac{\pi \cdot m_n}{2} & s_{os} &= \frac{\pi \cdot m_s}{2} \end{aligned}$$

Internal helical gears with corrected profile

a)- Without center distance variation

$$\begin{aligned} h_k &= m_n - x \cdot m_n \\ h_f &= \frac{7}{6} \cdot m_n + x \cdot m_n \quad \text{or} \quad h_f = \frac{5}{4} \cdot m_n + x \cdot m_n \\ s_{onc} &= \frac{m_n \cdot \pi}{2} - 2 \cdot x \cdot m_n \cdot \tan \alpha_{on} \\ s_{osc} &= \frac{m_s \cdot \pi}{2} - 2 \cdot x \cdot m_n \cdot \tan \alpha_{os} \end{aligned}$$

b)- With center distance variation

$$\begin{aligned} \text{inv } \alpha_{bs} &= \text{inv } \alpha_{os} + 2 \tan \alpha_{on} \frac{x_1 - x_2}{z_1 - z_2} \\ a_b &= a \frac{\cos \alpha_{os}}{\cos \alpha_{bs}} & d_b &= \frac{d_g}{\cos \alpha_{bs}} \\ s_{bs} &= r_b \left[\frac{S_{osc}}{r_o} - 2(\text{inv } \alpha_{os} - \text{inv } \alpha_{bs}) \right] \\ d_k &= m_n \left(\frac{z}{\cos \beta_o} - 2 + 2x \right) \end{aligned}$$

Contact length calculation

$$\begin{aligned} \rho_{k1} &= \sqrt{r_{k1}^2 - r_{g1}^2} & \rho_{k2} &= \sqrt{r_{k2}^2 - r_{g2}^2} \\ g &= \rho_{k1} - \rho_{k1} + a_b \cdot \sin \alpha_b \\ g_1 &= \rho_{k1} - r_{b1} \cdot \sin \alpha_b & g_2 &= -\rho_{k2} + r_{b2} \cdot \sin \alpha_b \end{aligned}$$

Contact radius R_a calculation

$$R_{a2} = \sqrt{(\rho_{k2} + g)^2 + r_{g2}^2}$$

In the case of helical gears use transverse section values α_{bs} instead of α_b .

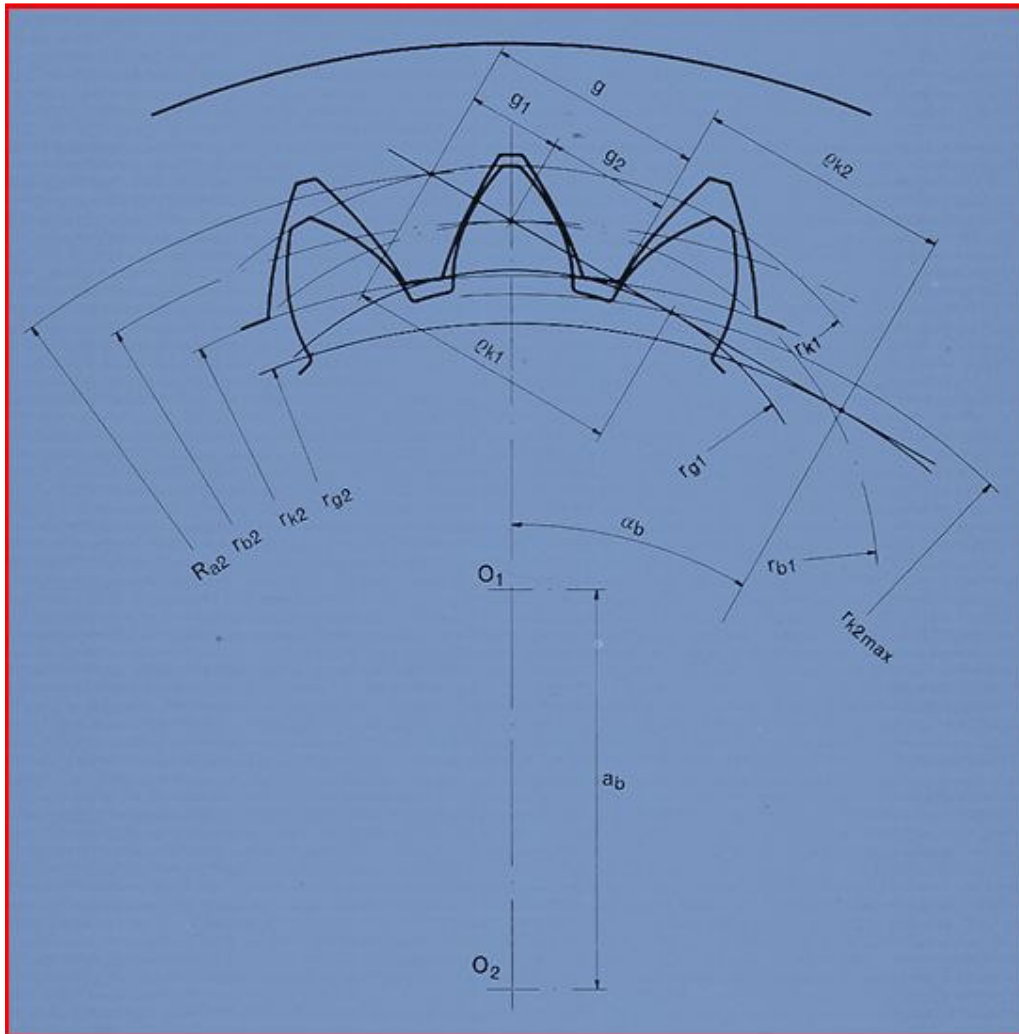


Fig. N°3

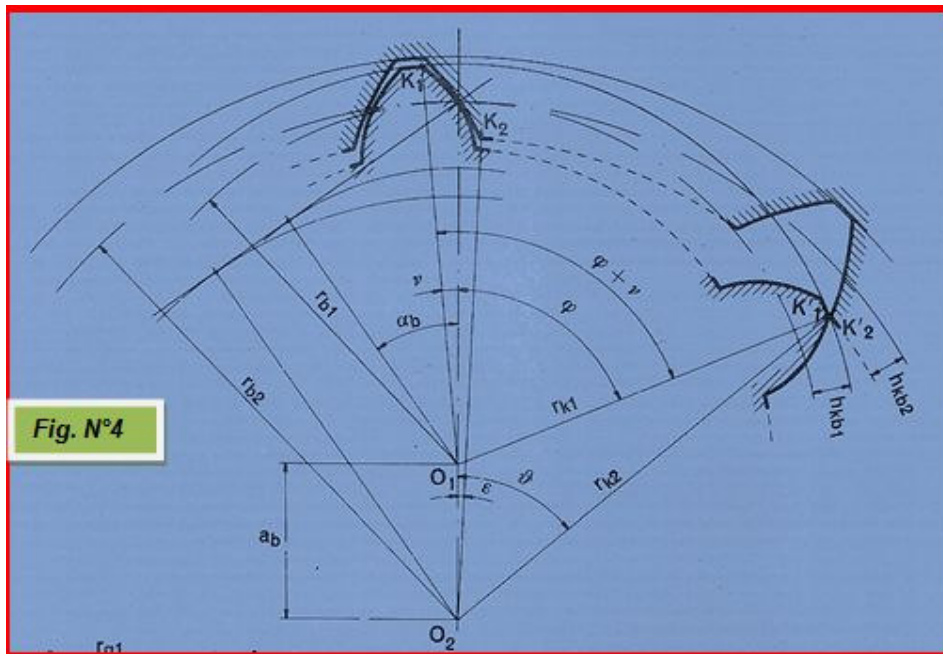
Interference

Primary interference

Minimum internal diameter without interference

$$d_{k2min} = \sqrt{d_g^2 + (2a_b \cdot \sin \alpha_b)^2}$$

Secondary interference (figure N°4)



$$\cos \delta = \frac{r_{g1}}{r_{k1}} \quad \nu = \text{inv } \delta - \text{inv } \alpha_b$$

$$\cos \delta = \frac{r_{k2}^2 + a_b^2 - r_{k1}^2}{2 \cdot r_{k2} \cdot a_b} \quad \cos \varphi = \frac{r_{k2}^2 - a_b^2 - r_{k1}^2}{2 \cdot r_{k1} \cdot a_b}$$

When the points K_1 and K_2 on the pinion and gear move to K'_1 and K'_2 in time t_1 and t_2 , the respective angles are:

$$\text{for the gear: } \delta - \varepsilon ; \quad t_2 = \frac{\delta - \varepsilon}{\omega_2}$$

$$\text{for the pinion: } \varphi + \nu ; \quad t_1 = \frac{\varphi + \nu}{\omega_1}$$

To avoid interference, the points K_1 and K_2 should not coincide at K'_1 and K'_2 and should satisfy the condition:

$$t_1 > t_2 \quad \text{or} \quad \frac{\varphi + \nu}{\omega_1} > \frac{\delta - \varepsilon}{\omega_2}$$

The diagram of figure N°5 is used to determine the largest difference $z_2 - z_1$, which is a function of the pressure angle α_0 and the ratio $\frac{h_k}{m}$, where not interference exist.

When the gears are corrected h_k becomes:

$$h_k = \frac{h_{kb2} + h_{kb1}}{2}$$

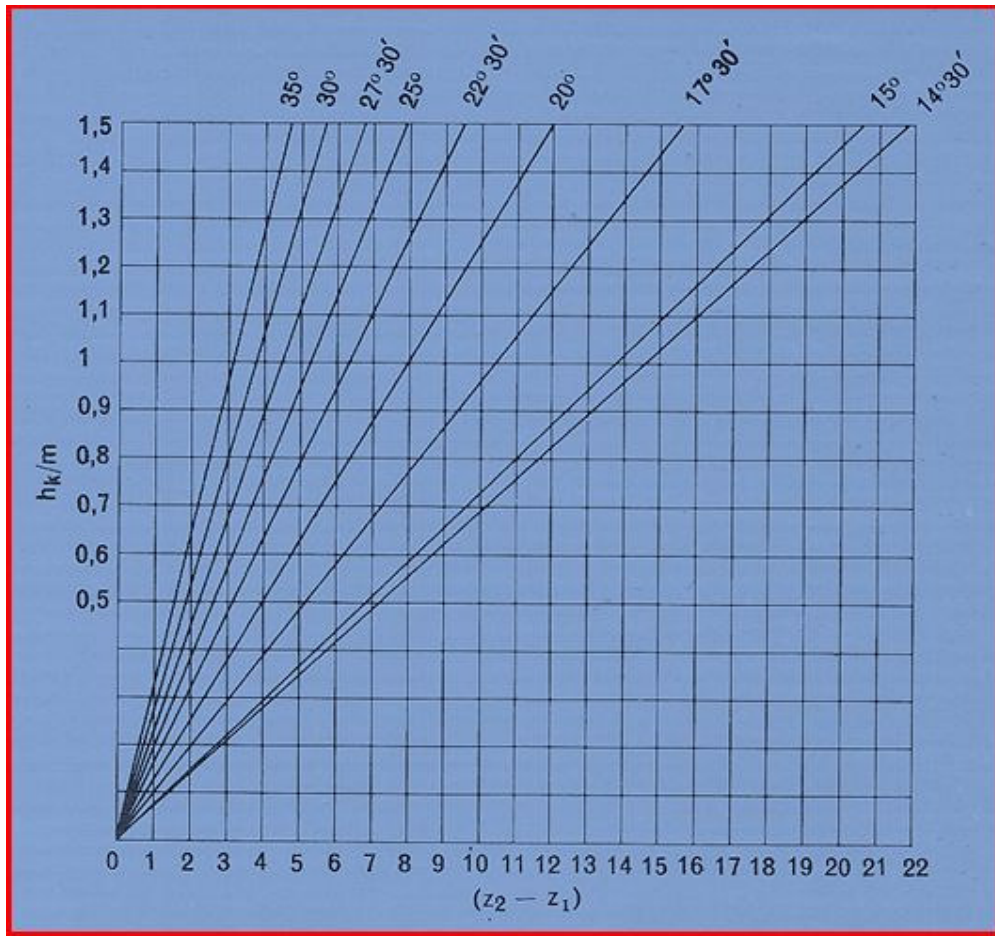


Fig. N°5

Dimension over pins and balls (figure N°6)

Spur gear with even number of teeth

$$\text{inv } \alpha_q = \text{inv } \alpha_o - \frac{d_r}{2r_o \cdot \cos \alpha_o} + \frac{l_o}{2r_o} \quad \text{from which we have } \alpha_q$$

$$r_q = r_o \frac{\cos \alpha_o}{\cos \alpha_q} \quad Q = 2 \cdot r_q - d_r$$

Spur gear with odd number of teeth

$$\alpha_q \text{ and } r_q \text{ are the same as for even teeth, but } Q = 2 \cdot r_q \cdot \cos \frac{\pi}{2z} - d_r$$

Helical gear with even number of teeth

$$\text{inv } \alpha_{qs} = \text{inv } \alpha_{os} - \frac{d_r}{2r_{os} \cdot \cos \beta_o \cos \alpha_{on}} + \frac{l_{os}}{2r_{os}}$$

$$r_{qs} = r_{os} \frac{\cos \alpha_{os}}{\cos \alpha_{qs}} \quad Q = 2 \cdot r_{qs} - d_r$$

Helical gear with odd number of teeth

α_{qs} and r_{qs} are the same as for even teeth, but

$$Q = 2 \cdot r_{qs} \cdot \cos \frac{\pi}{2z} - d_r$$

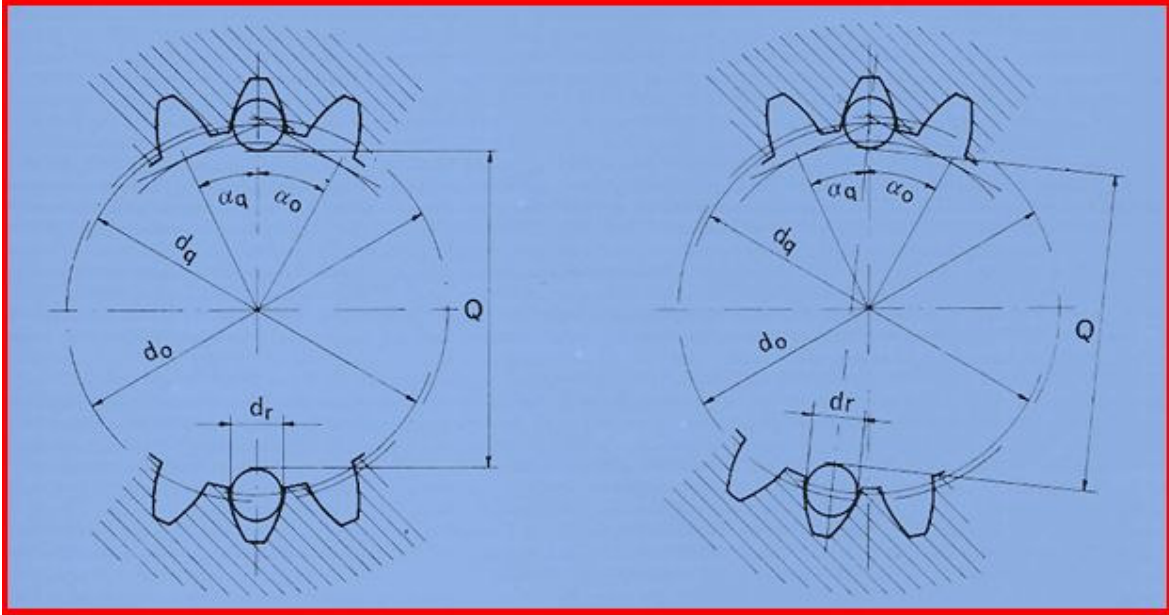


Fig.N°6